

02/02/00  
jc714 U.S. PRO

Patent  
Attorney's Docket No. 024444-729

jc511 U.S. PRO  
09/496200  
02/02/00

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

UTILITY PATENT  
APPLICATION TRANSMITTAL LETTER

Box PATENT APPLICATION  
Assistant Commissioner for Patents  
Washington, D.C. 20231

Sir:

Enclosed for filing is the utility patent application of Lisa PALMQVIST; Mikael LINDHOLM; Anders LENANDER; Björn LJUNGBERG; and Michael THYSELL for CEMENTED CARBIDE INSERT.

Also enclosed are:

- ☒ 1 sheet(s) of ☒ formal ☐ informal drawing(s);
- ☒ a claim for foreign priority under 35 U.S.C. §§ 119 and/or 365 is ☒ hereby made to SE 9900403-8 filed in SWEDEN on February 5, 1999; ☒ in the declaration;
- ☐ a certified copy of the priority document;
- ☐ a General Authorization for Petitions for Extensions of Time and Payment of Fees;
- ☐ statement(s) claiming small entity status;
- ☐ an Assignment document;
- ☐ an Information Disclosure Statement; and
- ☐ Other:
- ☒ An ☐ executed ☒ unexecuted declaration of the inventor(s) ☒ also is enclosed ☐ will follow.
- ☐ Please amend the specification by inserting before the first line the sentence --This application claims priority under 35 U.S.C. §§119 and/or 365 to      filed in      on     ; the entire content of which is hereby incorporated by reference.--
- ☐ A bibliographic data entry sheet is enclosed.



21839

☒ The filing fee has been calculated as follows [ ] and in accordance with the enclosed preliminary amendment:

CLAIMS					
	NO. OF CLAIMS		EXTRA CLAIMS	RATE	FEE
Basic Application Fee					\$690.00 (101)
Total Claims	20	MINUS 20 =	0	x \$18.00 (103)	0
Independent Claims	2	MINUS 3 =	0	x \$78.00 (102)	0
If multiple dependent claims are presented, add \$260.00 (104)					
Total Application Fee					690.00
If verified Statement claiming small entity status is enclosed, subtract 50% of Total Application Fee					
Add Assignment Recording Fee of if Assignment document is enclosed					
<b>TOTAL APPLICATION FEE DUE</b>					<b>690.00</b>

- [ ] This application is being filed without a filing fee. Issuance of a Notice to File Missing Parts of Application is respectfully requested.
- ☒ A check in the amount of \$ 690.00 is enclosed for the fee due.
- [ ] Charge \$ \_\_\_\_\_ to Deposit Account No. 02-4800 for the fee due.
- ☒ The Commissioner is hereby authorized to charge any appropriate fees under 37 C.F.R. §§ 1.16, 1.17 and 1.21 that may be required by this paper, and to credit any overpayment, to Deposit Account No. 02-4800. This paper is submitted in duplicate.

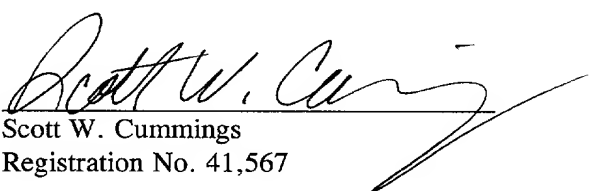
Please address all correspondence concerning the present application to:

Ronald L. Grudziecki  
Burns, Doane, Swecker & Mathis, L.L.P.  
P.O. Box 1404  
Alexandria, Virginia 22313-1404.

Respectfully submitted,

BURNS, DOANE, SWECKER & MATHIS, L.L.P.

Date: February 2, 2000

By:   
Scott W. Cummings  
Registration No. 41,567

P.O. Box 1404  
Alexandria, Virginia 22313-1404  
(703) 836-6620

0011952001020300

## CEMENTED CARBIDE INSERT

### BACKGROUND OF THE INVENTION

The present invention relates to a coated cutting tool insert particularly useful for turning of steel, like low alloyed steels, carbon steels and tough  
5 hardened steels, at high cutting speeds.

High performance cutting tools must nowadays possess high wear resistance, high toughness properties and good resistance to plastic deformation. This is particularly so when the cutting operation is carried out at very high cutting speeds and/or at high feed rates when large amount of heat is generated.

10 Improved resistance to plastic deformation of a cutting insert can be obtained by decreasing the WC grain size and/or by lowering the overall binder phase content, but such changes will simultaneously result in significant loss in the toughness of the insert.

Methods to improve the toughness behaviour by introducing a thick  
15 essentially cubic carbide free and binder phase enriched surface zone with a thickness of about 20-40  $\mu\text{m}$  on the inserts by so called gradient sintering techniques are in the art.

However, these methods produce a rather hard cutting edge due to a depletion of binder phase and enrichment of cubic phases along the cutting edge.

20 A hard cutting edge is more prone to chipping. Nevertheless, such carbide inserts

with essentially cubic carbide free and binder phase enriched surface zones are extensively used today for machining steel and stainless steel.

There are ways to overcome the problem with edge brittleness by controlling the carbide composition along the cutting edge by employing special  
5 sintering techniques or by using certain alloying elements, of which US 5,484,468, US 5,549,980, US 5,729,823 and US 5,643,658 are illustrated.

All these techniques give a binder phase enrichment in the outermost region of the edge. However, inserts produced according to these techniques often obtain micro plastic deformation at the outermost part of the cutting edge. In particular,  
10 this often occurs when the machining is carried out at high cutting speeds. A micro plastic deformation of the cutting edge will cause a rapid flank wear and hence a shortened lifetime of the cutting inserts. A further drawback of the above-mentioned techniques is that they are complex and difficult to fully control.

US 5,786,069 and US 5,863,640 disclose coated cutting tool inserts with a  
15 binder phase enriched surface zone and a highly W-alloyed binder phase.

### **SUMMARY**

The present invention provides a cutting tool insert for machining steel, including a cemented carbide body and a coating, wherein: the cemented carbide body includes WC, 2-10 wt.% of Co, 4-12 wt.% of cubic carbides of metals from  
20 groups 4, 5 or 6 of the periodic table, and N in an amount of between 0.9 and 1.7 % of the weight of the elements from groups 4 and 5; the cemented carbide body

includes a Co-binder phase which is highly alloyed with W, and has a CW-ratio of 0.75-0.90; the cemented carbide body has a surface zone with a thickness of  $<20\text{ }\mu\text{m}$ , which is binder phase enriched and essentially cubic carbide free; the cemented carbide body has a cutting edge which has a binder phase content which is 0.65-0.75 of the bulk binder phase content, and the binder phase content increases at a constant rate along a line which bisects said cutting edge, until it reaches the bulk binder phase content at a distance between 100 and 300  $\mu\text{m}$  from the cutting edge; and the coating includes a 3-12  $\mu\text{m}$  columnar TiCN layer followed by a 2-12  $\mu\text{m}$   $\text{Al}_2\text{O}_3$  layer, possibly with an outermost 0.5-4  $\mu\text{m}$  TiN layer.

The present invention also provides a method of making a cutting insert comprising a cemented carbide body having a binder phase, with a binder phase enriched surface zone and a binder phase depleted cutting edge, and a coating, including the steps of: forming a powder mixture including WC, 2-10 wt. % Co, 4-12 wt. % of cubic carbides of metals from groups 4, 5 or 6 of the periodic table, the binder phase having a CW-ratio of 0.75-0.90; adding N in an amount of between 0.9 and 1.7% of the weight of the elements from groups 4 and 5; mixing the powder with a pressing agent; milling and spray drying the mixture to a powder material compacting and sintering the powder material at a temperature of 1300-1500°C, in a controlled atmosphere of sintering gas at 40-60 mbar followed by cooling; applying post-sintering treatment; and applying a hard, wear resistant coating by CVD or MT-CVD-technique.

## **BRIEF DESCRIPTION OF THE DRAWING**

Figure 1 is a schematic drawing of a cross section of an edge of an insert gradient sintered according to the present invention.

## **5 DETAILED DESCRIPTION OF THE EMBODIMENTS**

It has now surprisingly been found that significant improvements with respect to resistance to plastic deformation and toughness behaviour can simultaneously be obtained for a cemented carbide insert if a number of features are combined. The improvement in cutting performance of the cemented carbide inserts can be obtained if the cobalt binder phase is highly alloyed with W, if the essentially cubic carbide free and binder phase enriched surface zone A has a certain thickness and composition, if the cubic carbide composition near the cutting edge B is optimised and if the insert is coated with a 3-12  $\mu\text{m}$  columnar TiCN-layer followed by a 2-12  $\mu\text{m}$  thick  $\text{Al}_2\text{O}_3$  layer, for example produced according to any of the patents US 5,766,782, US 5,654,035, US 5,674,564 or US 5,702,808, possibly with an outermost 0.5 - 4  $\mu\text{m}$  TiN-layer. The  $\text{Al}_2\text{O}_3$ -layer will serve as an effective thermal barrier during cutting and thereby improve not only the resistance to plastic deformation which is a heat influenced property but also increase the crater wear resistance of the cemented carbide insert. In addition, if the coating along the cutting edge is smoothed by an appropriate technique, like by brushing with a SiC-based nylon brush or by a gentle blasting

with  $\text{Al}_2\text{O}_3$  grains, the cutting performance can be enhanced further, in particular with respect to flaking resistance of the coating (see, e.g. US 5,851,210).

Said cutting insert possesses excellent cutting performance when machining steel at high cutting-speeds, in particular low alloyed steels, carbon steels and tough hardened steels. As a result a wider application area for the coated carbide insert is obtained because the cemented carbide insert according to the invention performs very well at both low and very high cutting speeds under both continuous and intermittent cutting conditions.

The coated cemented carbide insert of the invention has a  $< 20 \mu\text{m}$ , preferably  $5\text{-}15 \mu\text{m}$ , thick essentially cubic carbide free and binder phase enriched surface zone A (Fig. 1), preferably with an average binder phase content (by volume) of 1.2-3.0 times the bulk binder phase content. In order to obtain high resistance to plastic deformation but simultaneously avoid a brittle cutting edge the chemical composition is optimised in zone B (Fig. 1). Along line C (Fig. 1), in the direction from edge to the centre of the insert, the binder phase content increases essentially constantly until it reaches the bulk composition. At the edge the binder phase content by volume is 0.65-0.75, preferably about 0.7 times the binder phase content of the bulk. In a similar way, the cubic carbide phase content decreases along line C, preferably from about 1.3 times the content of the bulk. The depth of the binder phase depletion and cubic carbide enrichment along line C is  $100\text{-}300 \mu\text{m}$ , preferably  $150\text{-}250 \mu\text{m}$ .



The binder phase is highly W-alloyed. The content of W in the binder phase can be expressed as a

CW-ratio =  $M_s / (\text{wt. \% Co} * 0.0161)$  where  $M_s$  is the measured saturation magnetisation of the cemented carbide body in kA/m and wt-% Co is the weight percentage of Co in the cemented carbide. The CW-ratio takes a value  $\leq 1$  and the lower the CW-ratio, the higher is the W-content in the binder phase. It has now been found according to the invention that an improved cutting performance is achieved if the CW-ratio is 0.75-0.90, preferably 0.80-0.85.

Inserts according to the invention are further provided with a coating consisting of essentially 3-12  $\mu\text{m}$  columnar TiCN-layer followed by a 2-12  $\mu\text{m}$  thick  $\text{Al}_2\text{O}_3$ -layer deposited, for example according to any of the patents US 5,766,782, US 5,654,035, US 5,674,564, US 5,702,808 preferably with an  $\alpha$ - $\text{Al}_2\text{O}_3$ -layer, possibly with an outermost 0.5-4  $\mu\text{m}$  TiN-layer.

The present invention is applicable to cemented carbides with a composition of 2-10, preferably 4-7, weight percent of binder phase consisting of Co, and 4-12, preferably 7-10, weight percent cubic carbides of the metals from groups 4, 5 or 6 of the periodic table, preferably  $> 1$  wt. % of each Ti, Ta and Nb and a balance WC. The WC preferably has an average grain size of 1.0 to 4.0  $\mu\text{m}$ , more preferably 2.0 to 3.0  $\mu\text{m}$ . The cemented carbide body may contain small amounts,  $< 1$  volume %, of  $\eta$ -phase ( $\text{M}_6\text{C}$ ).

By applying layers with different thicknesses on the cemented carbide body according to the invention, the property of the coated insert can be optimised to

suit specific cutting conditions. In one embodiment, a cemented carbide insert produced according to the invention is provided with a coating of: 6  $\mu\text{m}$  TiCN, 8  $\mu\text{m}$   $\text{Al}_2\text{O}_3$  and 2  $\mu\text{m}$  TiN. This coated insert is particularly suited for cutting operation with high demand regarding crater wear. In another embodiment, a  
5 cemented carbide insert produced according to invention is provided with a coating of: 8  $\mu\text{m}$  TiCN, 4  $\mu\text{m}$   $\text{Al}_2\text{O}_3$  and 2  $\mu\text{m}$  TiN. This coating is particularly suited for cutting operations with high demands on flank wear resistance.

The invention also relates to a method of making cutting inserts comprising a cemented carbide substrate consisting of a binder phase of Co, WC and a cubic  
10 carbonitride phase with a binder phase enriched surface zone essentially free of cubic phase and a coating. The powder mixture consists 2-10, preferably 4-7, weight percent of binder phase consisting of Co, and 4-12, preferably 7-10, weight percent cubic carbides of the metals from groups 4, 5 or 6 of the periodic table, preferably > 1 wt.% of each Ti, Ta and Nb and a balance WC, preferably  
15 with an average grain size of 1.0-4.0  $\mu\text{m}$ , more preferably 2.0-3.0  $\mu\text{m}$ . Well-controlled amounts of nitrogen are added either through the powder as carbonitrides and/or added during the sintering process via the sintering gas atmosphere. The amount of added nitrogen will determine the rate of dissolution of the cubic phases during the sintering process and hence determine the overall  
20 distribution of the elements in the cemented carbide after solidification. The optimum amount of nitrogen to be added depends on the composition of the cemented carbide and in particular on the amount of cubic phases and varies

between 0.9 and 1.7%, preferably about 1.1-1.4%, of the weight of the elements from groups 4 and 5 of the periodic table. The exact conditions depend to a certain extent on the design of the sintering equipment being used. It is within the purview of the skilled artisan to determine whether the requisite surface zones A and B of cemented carbide have been obtained and to modify the nitrogen addition and the sintering process in accordance with the present specification in order to obtain the desired result.

The raw materials are mixed with pressing agent and possibly W such that the desired CW-ratio of the binder phase is obtained and the mixture is milled and spray dried to obtain a powder material with the desired properties. Next, the powder material is compacted and sintered. Sintering is performed at a temperature of 1300-1500°C, in a controlled atmosphere of between 40 and 60 mbar, preferably about 50 mbar, followed by cooling. After conventional post sintering treatments including edge rounding a hard, wear resistant coating, such as defined above, is applied by CVD- or MT-CVD-technique.

#### Example 1

A.) Cemented carbide turning inserts of the style CNMG120408-PM, DNMG150612-PM and CNMG160616-PR, with the composition 5.5 wt. % Co, 3.5 wt. % TaC, 2.3 wt. % NbC, 2.1 wt. % TiC and 0.4 wt. % TiN and balance WC with an average grain size of 2.5  $\mu\text{m}$  were produced according to the invention. The nitrogen was added to the carbide powder as TiCN. Sintering was done at

1450°C in a controlled atmosphere consisting of Ar, CO and some N<sub>2</sub> at a total pressure of about 50 mbar.

Metallographic investigation showed that the produced cemented carbide inserts had a cubic-carbide-free zone A with a thickness of 10 µm. Image analysis technique was used to determine the phase composition at zone B and the area along line C (Fig. 1). The measurements were done on polished cross sections of the inserts over an area of approx. 40 x 40 µm gradually moving along the line C. The phase composition was determined as volume fractions. The analysis showed that the cobalt content in zone B was 0.7 times the bulk cobalt content and the cubic carbide content 1.3 times the bulk gamma phase content. The measurements of the bulk content were also done by image analysis technique. The Co-content was gradually increasing and the cubic carbide content gradually decreasing along line C in the direction from the edge to the centre of the insert.

Magnetic saturation values were recorded and used for calculating CW-values. An average CW-value of 0.84 was obtained.

B.) Inserts from A were first coated with a thin layer < 1 µm of TiN followed by 6 µm thick layer of TiCN with columnar grains by using MT-CVD-techniques (process temperature 850°C and CH<sub>3</sub>CN as the carbon/nitrogen source). In a subsequent process step during the same coating cycle, an 8 µm thick α-Al<sub>2</sub>O<sub>3</sub> layer was deposited according to patent US 5,654,035. On top of the α-Al<sub>2</sub>O<sub>3</sub> layer a 1.5 µm TiN layer was deposited.

C.) Inserts from A were first coated by a thin layer  $< 1 \mu\text{m}$  of TiN followed by a  $9 \mu\text{m}$  thick TiCN-layer and a  $5 \mu\text{m}$  thick  $\alpha\text{-Al}_2\text{O}_3$  layer and a  $2 \mu\text{m}$  thick TiN layer on top. The same coating procedures as given in A.) were used.

D.) Commercially available cutting insert in style CNMG120408-PM,  
5 DNMG150612-PM and CNMG160616-PR, with the composition given below were used as references in the cutting tests:

Composition: Co = 5.5 wt. %, TaC = 5.5 wt. %, NbC = 2.3 wt. %, TiC  
= 2.6 wt. % and balance WC with a grain size  $2.6 \mu\text{m}$ . Cobalt enriched  
gradient zone: none

10 CW-ratio:  $> 0.95$

Coating:  $8 \mu\text{m}$  TiCN,  $6 \mu\text{m}$   $\text{Al}_2\text{O}_3$ ,  $0.5 \mu\text{m}$  TiN on top

E.) Inserts with the same cemented carbide composition as in D were coated with  $4 \mu\text{m}$  TiN and  $6 \mu\text{m}$   $\text{Al}_2\text{O}_3$ . Inserts styles CNMG120408-QM and CNMG120412-MR.

15 F.) Inserts in styles CNMG120408-QM and CNMG120412-MR with the composition: 4.7 wt. % Co, 3.1 wt. % TaC, 2.0 wt. % NbC, 3.4 wt. %, TiC 0.2 wt. % N and rest WC with a grain size of  $2.5 \mu\text{m}$  were produced. The inserts were sintered according to the method described in patent US 5,484,468, i.e., a method that gives cobalt enrichment in zone B. The sintered carbide inserts had a  
20  $25 \mu\text{m}$  thick gradient zone essentially free from cubic carbide. The inserts were coated with the same coating as in E.

### Example 2

Inserts from B and C of Example 1 were tested and compared with inserts from D with respect to toughness in a longitudinal. turning operation with interrupted cuts.

5           Material: Carbon steel SS1312.

          Cutting data:

                  Cutting speed =       140 m/min

                  Depth of cut =       2.0 mm

                  Feed = Starting with 0.12 mm and gradually increased by 0.08  
10       mm/min until breakage of the edge

                  15 edges of each variant were tested

                  Inserts style: CNMG120408-PM

          Results:

		mean feed at breakage
15	Inserts B	0.23 mm/rev
	Inserts C	0.23 mm/rev
	Inserts D	0.18 mm/rev

### Example 3

Inserts from B, C and D of Example 1 were tested with respect to resistance to plastic deformation in longitudinal turning of alloyed steel (AISI 4340).

5           Cutting data:

Cutting speed =	160 m/min
Feed =	0.7 mm/rev.
Depth of cut =	2 mm
Time in cut =	0.50 min

10           The plastic deformation was measured as the edge depression at the nose of the inserts.

Results:	Edge depression, $\mu\text{m}$
Insert B	43
Insert C	44
15       Insert D	75

Examples 2 and 3 show that the inserts B and C according to the invention exhibit much better plastic deformation resistance in combination with somewhat better toughness behaviour in comparison to the inserts D according to prior art.

#### Example 4

Inserts from E and F of Example 1 were tested with respect to flank wear resistance in longitudinal turning of ball bearing steel SKF25B.

Cutting data:

5	Cutting speed:	320 m/min
	Feed:	0.3 mm/rev.
	Depth of cut:	2 mm

Tool life criteria: Flank wear  $> 0.3$  mm

Results:

10		Tool life
	Insert E	8 min
	Insert F	6 min

Variant F exhibited micro plastic deformation resulting in more rapid development of the flank wear.

#### 15 Example 5

Inserts from E and F of Example 1 in inserts style CNMG120412-MR were tested at an end-user in machining of a steel casting component.

Cutting data:

Cutting speed:	170-180 m/min
----------------	---------------



Feed: 0.18 mm/rev.

Depth of cut: 3 mm

The component had the shape of a ring. The inserts machined two components each and the total time in cut was 13.2 min.

5 After the test the flank wear of the inserts were measured.

Results:

	Flank wear
Insert E	0.32 mm
Insert F	0.60 mm

10 Example 4 and 5 illustrate the detrimental effect of cobalt enrichment in the edge area B typical for inserts produced by prior art gradient sintering technique as described in e.g. US 5,484,468.

#### Example 6

15 Inserts from B and D from Example 1 were tested under the same condition as in Example 4. Inserts style CNMG120408-PM

Cutting data:

Cutting speed: 320 m/min

Feed: 0.3 mm/rev.

Depth of cut: 2 mm

Tool life criteria: Flank wear  $>0.3$  mm

Results:	Tool life
Insert B	8 min
Insert D	8 min

5     Example 7

Inserts from B and D of Example 1 were tested at an end user in the machining of cardan shafts in tough hardened steel. Insert style DNMG150612-PM.

Cutting condition:

10	Cutting speed:	150 m/min
	Feed:	0.3 mm/rev.
	Depth of cut:	3 mm

The inserts machined 50 component each. Afterwards the flank wear of the inserts was measured.

15	Results:	
		Flank wear
	Insert B	0.15 mm
	Insert D	0.30 mm

Examples 6 and 7 illustrate that inserts with an optimised edge zone composition according to the invention do not suffer from micro plastic deformation and hence no rapid flank wear as prior art gradient sintered insert F does (see examples 4 and 5).

5     Example 8

In a test performed at an end-user inserts from B, C and D in Example 1 in style CNMG160616-PR were run in a longitudinal turning operation in machining of crankshaft in low alloyed steel.

10     The inserts were allowed to machine 90 crankshafts and the flank wear was measured and compared.

       Cutting data:

Cutting speed:	220 m/min
Feed:	0.6 mm/rev.
Depth of cut:	3-5 mm
15       Total time in cut:	27 min.

The dominating wear mechanism was plastic deformation of the type edge impression causing a flank wear.

       Results:

	Flank wear
20       Insert B	0.2 mm



**WHAT IS CLAIMED IS:**

1. A cutting tool insert for machining steel, comprising a cemented carbide body and a coating, wherein:

the cemented carbide body comprises WC, 2-10 wt. % Co, 4-12 wt. % of  
5 cubic carbides of metals from groups 4, 5 or 6 of the periodic table, and N in an  
amount of between 0.9 and 1.7% of the weight of the elements from groups 4 and  
5;

the cemented carbide body comprises a Co-binder phase which is highly  
alloyed with W, and has a CW-ratio of 0.75-0.90;

10 the cemented carbide body has a surface zone with a thickness of  $< 20 \mu\text{m}$ ,  
which is binder phase enriched and essentially cubic carbide free;

the cemented carbide body has a cutting edge which has a binder phase  
content of 0.65-0.75 by volume of the bulk binder phase content, and the binder  
phase content increases at a constant rate along a line which bisects said cutting  
15 edge until it reaches the bulk binder phase content at a distance between 100 and  
300  $\mu\text{m}$  from the cutting edge; and

the coating comprises a 3-12  $\mu\text{m}$  columnar TiCN layer followed by a  
2-12  $\mu\text{m}$   $\text{Al}_2\text{O}_3$  layer.

2. The cutting tool insert of claim 1, wherein the cemented carbide  
20 body comprises more than 1 wt. % of each Ti cubic carbide, Ta cubic carbide and  
Nb cubic carbide.

3. The cutting tool insert of claim 1, wherein the amount of N in the cemented carbide body is between 1.1 and 1.4% of the weight of the elements from groups 4 and 5.

4. The cutting tool insert of claim 1, wherein the binder phase content of the cutting edge of the cemented carbide body is 0.7 of the bulk binder phase content of the cemented carbide body.

5. The cutting tool insert of claim 1, wherein the distance from the cutting edge at which the binder phase content reaches the bulk binder phase content is between 150 and 250  $\mu\text{m}$ .

6. The cutting tool insert of claim 1, wherein the surface zone of the cemented carbide body is 5-15  $\mu\text{m}$  thick.

7. The cutting tool insert of claim 1, wherein the cemented carbide body comprises 4-7 wt. % Co and 7-10 wt. % of the specified cubic carbides.

8. The cutting tool insert of claim 1, wherein the  $\text{Al}_2\text{O}_3$  coating layer is  $\alpha\text{-Al}_2\text{O}_3$ .

9. The cutting tool insert of claim 1, which has an outermost coating layer of TiN.

10. The cutting tool insert of claim 1, wherein the average WC-grain size is between 2.0 and 3.0 $\mu$ m.

5 11. A method of making a cutting insert comprising a cemented carbide body having a binder phase, with a binder phase enriched surface zone, and a binder phase depleted cutting edge, and a coating, comprising the steps of:

forming a powder mixture containing WC, 2-10 wt. % Co, 4-12 wt. % of cubic carbides of metals from groups 4, 5 or 6 of the periodic table, the binder  
10 phase having a CW-ratio of 0.75-0.90;

adding N in an amount of between 0.9 and 1.7% of the weight of the elements from groups 4 and 5;

mixing said powder with a pressing agent;

milling and spray drying the mixture to a powder material;

15 compacting and sintering the powder material at a temperature of 1300-1500°C, in a controlled atmosphere of sintering gas at 40-60 mbar followed by cooling;

applying post-sintering treatment; and

applying a hard, wear resistant coating by CVD- or MT-CVD-technique.

12. The method of claim 11, wherein the powder mixture comprises 2-7 wt. % Co.

13. The method of claim 11, wherein the powder mixture comprises 7-10 wt. % of cubic carbides of the metals from groups 4, 5 or 6 of the periodic table.

14. The method of claim 11, wherein the powder mixture comprises more than 1 wt. % of each Ti cubic carbide, Ta cubic carbide and Nb cubic carbide.

15. The method of claim 11, wherein N is added in an amount between 1.1 and 1.4% of the weight of elements from groups 4 and 5.

16. The method of claim 11, wherein N is added to the powder mixture as a carbonitride.

17. The method of claim 11, wherein the N is added during the sintering step as part of the sintering gas atmosphere.

18. The method of claim 11, wherein the sintering is carried out at about 50 mbar.



19. The method of claim 11, wherein the hard, wear resistant coating is a 3-12  $\mu\text{m}$  columnar TiCN layer followed by a 2-12  $\mu\text{m}$   $\text{Al}_2\text{O}_3$ .

20. The method of claim 11, wherein W is added to the powder mixture with the pressing agent, so as to achieve the CW-ratio of 0.75-0.90.

## **ABSTRACT OF THE DISCLOSURE**

The present invention relates to a coated cemented carbide insert for turning of steel, like low alloyed steels, carbon steels and tough hardened steels at high cutting speeds. The cemented carbide consists of WC, 2-10 wt. % Co and 4-12 wt. % of cubic carbides of metals from groups 4, 5 or 6 of the periodic table, preferably Ti, Ta and Nb. The Co-binder phase is highly alloyed with W with a CW-ratio of 0.75-0.90. The insert has a binder phase enriched and essentially cubic carbide free surface zone A of a thickness of  $< 20 \mu\text{m}$  and along a line C essentially bisecting the edge, in the direction from the edge to the centre of the insert, a binder phase content increases essentially monotonously until it reaches the bulk composition. The binder phase content at the edge is 0.65-0.75 times the binder phase content by volume of the bulk and the depth of the binder phase depletion is 100-300  $\mu\text{m}$ , preferably 150-250  $\mu\text{m}$ . The insert is coated with 3-12  $\mu\text{m}$  columnar TiCN-layer followed by a 2-12  $\mu\text{m}$  thick  $\text{Al}_2\text{O}_3$ -layer.

002020" 002020" 002020"

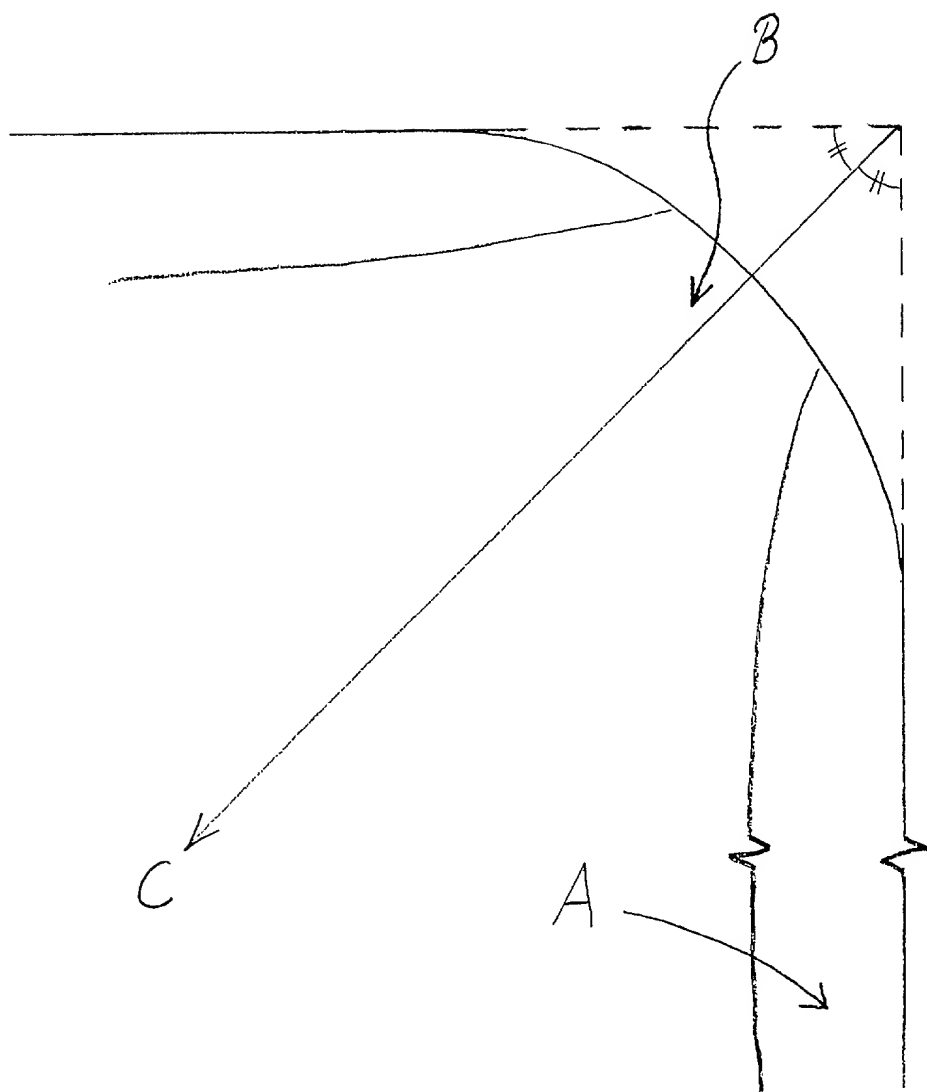


Fig. 1

**COMBINED DECLARATION AND POWER OF ATTORNEY  
FOR UTILITY PATENT APPLICATION**

Attorney's Docket No.

024444-729

As a below-named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name;

I BELIEVE I AM THE ORIGINAL, FIRST AND SOLE INVENTOR (if only one name is listed below) OR AN ORIGINAL, FIRST AND JOINT INVENTOR (if more than one name is listed below) OF THE SUBJECT MATTER WHICH IS CLAIMED AND FOR WHICH A PATENT IS SOUGHT ON THE INVENTION ENTITLED:

CEMENTED CARBIDE INSERT

the specification of which

(check one)

☐

is attached hereto;

☒

was filed on February 2, 2000 as

Application No. \_\_\_\_\_

and was amended on \_\_\_\_\_;  
(if applicable)

I HAVE REVIEWED AND UNDERSTAND THE CONTENTS OF THE ABOVE-IDENTIFIED SPECIFICATION, INCLUDING THE CLAIMS, AS AMENDED BY ANY AMENDMENT REFERRED TO ABOVE;

I ACKNOWLEDGE THE DUTY TO DISCLOSE TO THE OFFICE ALL INFORMATION KNOWN TO ME TO BE MATERIAL TO PATENTABILITY AS DEFINED IN TITLE 37, CODE OF FEDERAL REGULATIONS, Sec. 1.56 (as amended effective March 16, 1992);

I do not know and do not believe the said invention was ever known or used in the United States of America before my or our invention thereof, or patented or described in any printed publication in any country before my or our invention thereof or more than one year prior to said application; that said invention was not in public use or on sale in the United States of America more than one year prior to said application; that said invention has not been patented or made the subject of an inventor's certificate issued before the date of said application in any country foreign to the United States of America on any application filed by me or my legal representatives or assigns more than twelve months prior to said application;

I hereby claim foreign priority benefits under Title 35, United States Code Sec. 119 and/or Sec. 365 of any foreign application(s) for patent or inventor's certificate as indicated below and have also identified below any foreign application for patent or inventor's certificate on this invention having a filing date before that of the application(s) on which priority is claimed:

**COMBINED DECLARATION AND POWER OF ATTORNEY**

Attorney's Docket No.

024444-729

COUNTRY/INTERNATIONAL	APPLICATION NUMBER	DATE OF FILING (day, month, year)	PRIORITY CLAIMED
SWEDEN	SE 9900403-8	5 February 1999	YES <u>X</u> NO <u>  </u>
			YES <u>  </u> NO <u>  </u>

I hereby appoint the following attorneys and agent(s) to prosecute said application and to transact all business in the Patent and Trademark Office connected therewith and to file, prosecute and to transact all business in connection with international applications directed to said invention:

William L. Mathis	17,337	R. Danny Huntington	27,903	Gerald F. Swiss	30,113
Robert S. Swecker	19,885	Eric H. Weisblatt	30,505	Michael J. Ure	33,089
Platon N. Mandros	22,124	James W. Peterson	26,057	Charles F. Wieland III	33,096
Benton S. Duffett, Jr.	22,030	Teresa Stanek Rea	30,427	Bruce T. Wieder	33,815
Norman H. Stepno	22,716	Robert E. Krebs	25,885	Todd R. Walters	34,040
Ronald L. Grudziecki	24,970	William C. Rowland	30,888	Ronni S. Jillions	31,979
Frederick G. Michaud, Jr.	26,003	T. Gene Dillahunt	25,423	Harold R. Brown III	36,341
Alan E. Kopecki	25,813	Patrick C. Keane	32,858	Allen R. Baum	36,086
Regis E. Slutter	26,999	Bruce J. Boggs, Jr.	32,344	Steven M. du Bois	35,023
Samuel C. Miller, III	27,360	William H. Benz	25,952	Brian P. O'Shaughnessy	32,747
Robert G. Mukai	28,531	Peter K. Skiff	31,917	Kenneth B. Leffler	36,075
George A. Hovanec, Jr.	28,223	Richard J. McGrath	29,195	Fred W. Hathaway	32,236
James A. LaBarre	28,632	Matthew L. Schneider	32,814		
E. Joseph Gess	28,510	Michael G. Savage	32,596		

**21839**

and:

Address all correspondence to:

**21839**

Ronald L. Grudziecki  
BURNS, DOANE, SWECKER & MATHIS, L.L.P.  
P.O. Box 1404  
Alexandria, Virginia 22313-1404

Address all telephone calls to: Ronald L. Grudziecki at (703) 836-6620.

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

FULL NAME OF SOLE OR FIRST INVENTOR	SIGNATURE	DATE
Lisa PALMQVIST		
RESIDENCE	CITIZENSHIP	
Göteborg, SWEDEN	SWEDISH	
POST OFFICE ADDRESS		
Helenebergagatan, Villa Corinne, 412 62, Göteborg, SWEDEN		
FULL NAME OF SECOND JOINT INVENTOR, IF ANY	SIGNATURE	DATE
Mikael LINDHOLM		
RESIDENCE	CITIZENSHIP	
Hägersten, SWEDEN	SWEDISH	
POST OFFICE ADDRESS		
Cedergrensvägen 25, 126 36, Hägersten, SWEDEN		

<b>COMBINED DECLARATION AND POWER OF ATTORNEY</b>	Attorney's Docket No.
	024444-729

FULL NAME OF THIRD JOINT INVENTOR, IF ANY	SIGNATURE	DATE
Anders LENANDER		
RESIDENCE	CITIZENSHIP	
Tyresö, SWEDEN	SWEDISH	
POST OFFICE ADDRESS		
Sofiebergsv. 33 A, 135 53 Tyresö, SWEDEN		
FULL NAME OF FOURTH JOINT INVENTOR, IF ANY	SIGNATURE	DATE
Björn LJUNGBERG		
RESIDENCE	CITIZENSHIP	
Enskede, SWEDEN	SWEDISH	
POST OFFICE ADDRESS		
Kulstötärvägen 96, 122 44 Enskede, SWEDEN		
FULL NAME OF FIFTH JOINT INVENTOR, IF ANY	SIGNATURE	DATE
Michael THYSELL		
RESIDENCE	CITIZENSHIP	
Stockholm, SWEDEN	SWEDISH	
POST OFFICE ADDRESS		
Grev Turegatan 82, 114 38, Stockholm, SWEDEN		

002020 " 00295"